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Abstract

It is shown that in NIMROD the formation of closed current configurations, occurring only after the voltage is turned off, is due to the faster resistive decay of non-symmetric modes compared to the symmetric projection of the 3D steady state achieved by gun injection. Implementing Spitzer resistivity is required to make a definitive comparison with experiment, using two experimental signatures of the model discussed in the paper. If there are serious disagreements, it is suggested that a phenomenological hyper-resistivity be added to the $n = 0$ component of Ohm's law, similar to hyper-resistive Corsica models that appear to fit experiments. Hyper-resistivity might capture physics at small scale missed by NIMROD. Encouraging results would motivate coupling NIMROD to SPICE with edge physics inspired by UEDGE, as a tool for experimental data analysis.

1. NIMROD Results

We consider an example of pulsed injection, Run NIM.3-034, in pillbox geometry with constant resistivity. After the field builds up (to about 1T), the voltage is shut off (crowbar). At that time all lines are open. During decay, lines close within a radius $a(t)$ roughly centered on the symmetric magnetic axis, as shown in Figures 1 - 2 at sequential intervals Δt after crowbar. The symmetric flux surfaces, shown in Figure 3, change little with time. Table 1 gives the approximate closure radius and the $n = 0$ and $n = 1$ magnetic energies ($E_{1,2}$) and the $n = 0$ kinetic energy (K_o) and total K at various intervals Δt . Complete histories are plotted in Figure 4.

Table 1. NIMROD Decay History

$\Delta t(\text{ms})$	$E_o(\text{MJ})$	$E_1(\text{MJ})$	$K_o(\text{J})$	$K(\text{J})$	$a(t)/(R/2)$
0	2.1	0.1	300	375	open
5.6	1.8	0.09	2.3	3.4	open
14.4	1.6	0.08	1.75	2.7	≈ 0.5
28.9	1.3	0.05	1.5	2	≈ 0.5

2. Interpretation

The magnetic energies E_0 and E_1 decay approximately exponentially, with time constants:

$$\begin{aligned}\tau_0 &= 60.3 \text{ ms} & n = 0 \text{ decay} \\ \tau_1 &= 41.7 \text{ ms} & n = 1 \text{ decay}\end{aligned}$$

The symmetric state decay time τ_0 is to be compared with the decay time for the lowest Taylor state in a closed flux conserver (no bias), given by:

$$\tau = (2\eta\lambda_0^2/\mu_0)^{-1} = 80 \text{ ms} \quad (1)$$

where $\eta = 0.25\mu_0$ and $R = 1\text{m}$ (lowest $\lambda_0 = 5$).

That E_0 and E_1 decay exponentially indicates that they are no longer coupled by instability in decay. We can see this using the spectral formulation of incompressible resistive MHD, in which the system can be described by symmetric and perturbation fields B_0 and B_1 , the perturbed velocity v_1 , and the driven flux core field B_{FC} , giving:

$$\begin{aligned}d(1/2 B_{FC}^2)/dt &= S B_{FC} & - & M_{FC} v_1 B_1 B_{FC} - (B_{FC}^2/2\tau_{FC}) \quad (2) \\ &\rightarrow & & \downarrow\end{aligned}$$

$$\begin{aligned}dE_1/dt &= -M_0 v_1 B_1 B_0 & + & M_{FC} v_1 B_1 B_{FC} - E_1/\tau_1 \quad (3) \\ &\downarrow & & \end{aligned}$$

$$d(1/2 B_0^2)/dt = M_0 v_1 B_1 B_0 - (B_0^2/2\tau_0) \quad (4)$$

with $E_1 = 1/2 (\rho v_1^2 + B_1^2/\mu_0)$. The steady state existing at $\Delta t = 0$ is given crudely by:

$$\rho v_1^2 + B_1^2/\mu_0 = f B_0^2/\mu_0 \quad \text{free energy} \quad (5)$$

$$v_1 B_1 = (1/M_0 \lambda_0 \tau_0) B_0 \quad \text{from Eq. (4)} \quad (6)$$

There are two solutions. The one with the smaller value of $v_1 = (1/M_0 \lambda_0 \tau_0 \sqrt{f}) \approx (1/M_0 S \sqrt{f}) v_{ALFVEN}$ corresponds to that given by NIMROD ($K \ll E_1$).

Here arrows indicate the direction of energy flow in the driven state. The velocity v_1 plays a crucial role, whereby the source S (voltage) drives the dynamo $v_1 B_1$ by Eq. (2), which drives the velocity by Eq. (3), which drives B_0 by Eq. (4). The rapid decay of v_1

($\propto \sqrt{K}$) after crowbar kills the coupling, giving the observed exponential decay of the magnetic energies at rates like Eq. (1) but with different λ 's for different modes.

3. Effect of Temperature on Decay and Reconnection

Including ohmic heating and heat transport together with Spitzer resistivity will affect the above results in several ways:

a. When closure occurs, ohmic heating will increase the temperature there, as shown in Figure 5 (for arbitrary $\kappa_{||} = 100\kappa_{\perp}$). In future calculations with Spitzer resistivity, this should cause the closed flux to decay more slowly than the open field lines. Closure occurs by the decay of B_1/B_0 (since B_0 alone is closed). With constant η , only small differences in λ_0^2 and λ_1^2 cause this ratio to decrease, while averaging a temperature-dependent η over these states may relatively enhance the decay of B_1 .

b. Faster decay on the open lines, and on outer surfaces of the closed flux, will cause the λ profile to sag (observed in experiments), which may trigger MHD instability during decay (also sometimes observed). In the absence of instability, the only process attempting to maintain the λ profile is induction due to decay of the field. Induction due to slow decay of the interior toroidal field cannot sustain the rapidly decaying peripheral poloidal current - including the gun current on open field lines.

c. Delayed closure will delay any rise in temperature and allow the rapid decay of the field everywhere. Closure slow compared to the open line decay time (τ in Eq. (1) with temperature for open lines) will lead to the same result, since most of the energy would be lost during closure.

4. Model

These observations suggest a model of pulsed injection in NIMROD, described by the following hypotheses:

a. During buildup field lines are open. Instability during buildup is essentially ideal MHD, which preserves open field lines, giving unit current amplification.

b. MHD mode growth saturates in a stable quasi-steady state, probably with a λ profile peaked at the geometric axis, with a slope near a stability threshold.

c. Closure happens during resistive decay, not by instability but by the faster decay of non-symmetric modes relative to the symmetrically averaged state, which has closed surfaces. These non-symmetric modes include sheet currents generated during unstable

growth to preserve open lines. (For tearing modes, the sheets have finite width and instability and closure can occur simultaneously, both at resistive rates.)

d. Stable decay is caused by a window of stability, between the marginal profile peaked on the geometric axis achieved by injection, and an oppositely sloped profile peaked at the magnetic axis. However, with Spitzer resistivity, the λ profile should begin to “sag” at the outer edge, since induction cannot sustain the profile at the outer edge, as noted previously. Eventually the sagging λ profile may trigger instability again, which could be observed in NIMROD.

5. Predictions

The above model provides a qualitative description of NIMROD that can be quantified by introducing the correct anisotropic heat transport and Spitzer resistivity. The model can be used to calculate the useful period for a pulsed reactor between closure and ultimate instability (if this occurs). Multipulse injection could also be calculated, to determine optimum timing allowing closure during decay but avoiding instability in decay.

Comparison of NIMROD results with experiment will shed light on the greatest uncertainty in the model -- the mechanism of closure. The main experimental signature of closure is a rise in temperature (more precisely, pressure) on closed surfaces, to a level determined by the beta that can be achieved by ohmic heating with ion classical or Rechester-Rosenbluth heat transport. A rise in temperature earlier than or higher than that predicted by NIMROD would be a clear signal that non MHD mechanisms cause closure (or at least modes not accessible by NIMROD).

The other important feature of the above model is the fact that the system becomes stable during saturation and decay, allowing a decoupling of the decaying spheromak and decaying gun current. There are two experimental signatures of this prediction. One would be a field decay time that increases as the core temperature increases -- one of the hallmark observations in CTX. The other would be a decay of the gun current faster than the field. To quantify the latter, the maximum gun current that could be sustained inductively by a stable decaying spheromak would be a small fraction of that in steady state, $I_{GUN}(0)$, of the order of the ratio of decay times for the open-line gun current and the spheromak, given by:

$$I_{GUN} = (3/10)(V/R_{\Omega}) \approx (3/10)(T_E/T) I_{GUN}(0) \quad (7)$$

where V is the loop voltage due to the slowly decaying spheromak toroidal current I_{TOR} reduced by 3/10 to account for the sheath; R_{Ω} is the open line resistance excluding the sheath; T_E is the open line temperature; and T is the spheromak core temperature.

The changes in equilibrium as the gun current decays away are illustrated by Corsica results in Figures 7 and 8, for the bias configuration shown in Figure 6. In Figure 7, λ is flat, being the same inside and outside the separatrix, giving a gun current comparable to the toroidal current. In Figure 8, λ is zero outside the separatrix giving zero gun current, rising to a maximum at the magnetic axis inside the separatrix (sagging profile). Note that the location of the spheromak inside the flux conserver is little changed when the gun current goes away -- a fact that persists to very small confined toroidal current relative to a fixed bias. The equilibrium at zero gun current is characterized by zero toroidal field at the separatrix and a poloidal field there matched to that produced by the bias flux compressed in the flux core.

6. Gun Efficiency

Aside from sheath loss and other external effects during injection that are not included in NIMROD pillbox calculations, instability occurring in NIMROD (probably ideal MHD) is very efficient at converting injected energy into the symmetric component -- about 95% going into E_o (mostly the closed spheromak) at crowbar in Table 1. This would be the internal gun efficiency except for energy lost during closure.

The last data point $\Delta t = 28.9 \text{ ms} \approx 0.5 \tau$, at which time 67% of the E_o energy remains and the closure radius is about half the spheromak minor radius. How long full closure will take in NIMROD remains to be seen.

An estimate of the importance of fast closure compared to τ (for open lines) is illustrated by the following model describing decay of the magnetic energy on open lines as the radius of closure $a(t)$ grows in time:

$$dB^2/dt = - (B^2/\tau) \{ 1 - (a(t)/(R/2))^2 \} \quad (8)$$

In principle $a(t)$ could be obtained from NIMROD, by fitting data like that given in Table 1. Lacking sufficient data to obtain a good fit, here we illustrate the point assuming $a(t)/(R/2) = [1 - \exp(-t/\tau_c)]$ with closure time τ_c , giving:

$$B^2(t)/B^2(0) \rightarrow \exp\{-3/2 (\tau_c/\tau)\} \quad \text{for } t \gg \tau_c \quad (9)$$

Thus most of the energy would be lost during closure unless $\tau_c < \tau$ on open lines.

It will also matter when closure occurs. This is illustrated in Figure 9, showing SPHERE calculations approximating a single pulse injection by the SSPX Formation Bank.

In these calculations delayed closure is approximated by holding the temperature fixed at a low value up to a delay time, after which the usual SPHERE heat transport calculation begins. Four cases are shown, Case 1 with no delay and three other cases with progressively longer delays. Temperatures are in KeV, with B in tesla. Evidently prolonging ohmic loss at a low temperature during the buildup limits the field and hence the ultimate temperature achieved.

Finally, it matters whether NIMROD correctly calculated saturated MHD amplitudes. Earlier benchmarks of MHD codes found that including compressibility significantly affected MHD amplitudes.

7. Hyper-resistivity

If NIMROD results turn out to be inconsistent with experiment, it may be useful to implement into the symmetric Ohm's law a hyper-resistivity already shown to agree with experiment, of the form:

$$E_{||} = \eta j_{||} - \nabla \cdot \Lambda \nabla \lambda_{||} \quad (10)$$

The hyper-resistive correction should be added only to the $n = 0$ component of the Ohm's law as it appears in Faraday's law describing the time evolution of the magnetic field. Implementation would be similar to the hyper-resistive model in Corsica [1] except that in NIMROD it should be applied all the way to the wall including the open-line flux core. Then in effect NIMROD calculates helicity transport by the "dough-hook" (or some symmetric instability) while Λ represents processes not in NIMROD.

Here, hyper-resistivity is intended to represent small-scale turbulence not accessible in NIMROD, such as closure effects at the ion Larmor radius scale, or pressure-driven tearing, followed by Rutherford resistive island growth over larger dimensions. We model this by:

$$\Lambda = C(T_E/T) \quad (11)$$

where C is a fitting constant scaled to the core temperature T at the magnetic axis calculated by NIMROD and T_E is the temperature at the outer "edge" (at $r = 0$ at the midplane). Aside from the rapid small scale closure process, this model is similar to "enhanced resistance" discussed in Ref. [2] and it is consistent with the observation that empirical fits of this kind to sustainment shots have succeeded fairly well, with the proviso that Λ is smaller at higher temperature [1].

The issue is whether hyper-resistivity significantly affects MHD modes that open the flux surfaces. With the model in Eq. (11), it could do so only through changes in the λ profile, in competition with MHD control of the profile. At the expected level based on results from Ref. [1], with Λ proportional to an appropriately-averaged resistivity, hyper-resistivity would have little effect prior to MHD saturation. However, it could aid closure during weak sustainment, by reducing the decay of the symmetric state, first during the late stages of buildup as modes saturate. The latter effect might also benefit closure in pulsed experiments like the Formation Bank. In the decay phase of a pulsed reactor, outward helicity propagation by hyper-resistivity might actually be harmful, by prolonging the coupling of the decaying spheromak to the gun current, but also helpful, by delaying the onset of MHD instability due to sagging λ .

There may be a logical inconsistency in assuming that short scale processes can give rise to resistive Rutherford island growth in an otherwise MHD stable regime (perhaps implying many close-spaced resonances missed by MHD). Note also that Eq. (11) differs from another ad hoc hyper-resistivity model in Ref. [3] in which Λ is proportional to non-symmetric MHD mode amplitudes, as a model of Rechester-Rosenbluth (R-R) momentum transport in a static tangled field produced by MHD. Even so, significant effects occurred only if Λ was larger than expected values based on R-R transport.

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References

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- [2] T. K. Fowler, D. D. Hua and B. W. Stallard, "Spheromak Impedance and Current Amplification," UCRL-ID-147087, January 31, 2002.
- [3] D. D. Hua, T. K. Fowler and E. C. Morse, *J. Plasma Phys.* **4**, 275 (2001).

Figure 1. NIMROD magnetic field line surface-of-section plot at $\Delta t=14.4$ ms after crowbar (nim3.034).

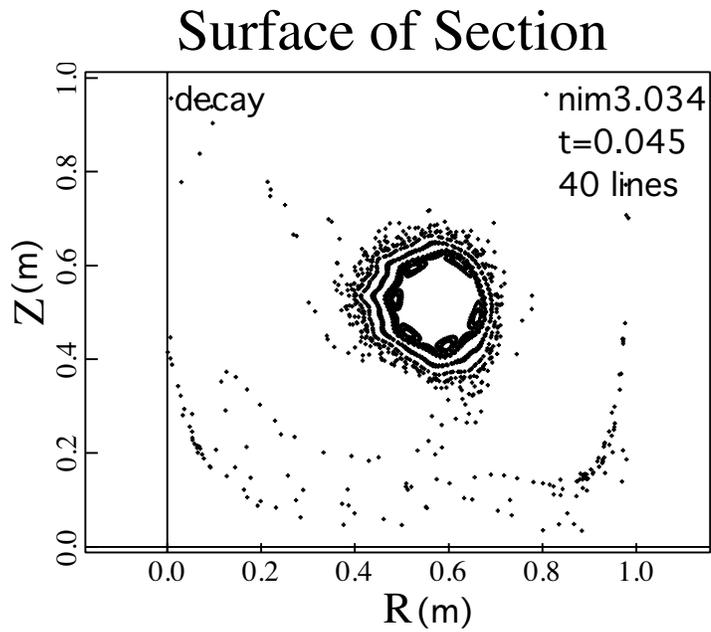


Figure2. NIMROD magnetic field line surface-of-section plot at $\Delta t=28.9$ ms after crowbar (nim3.034).

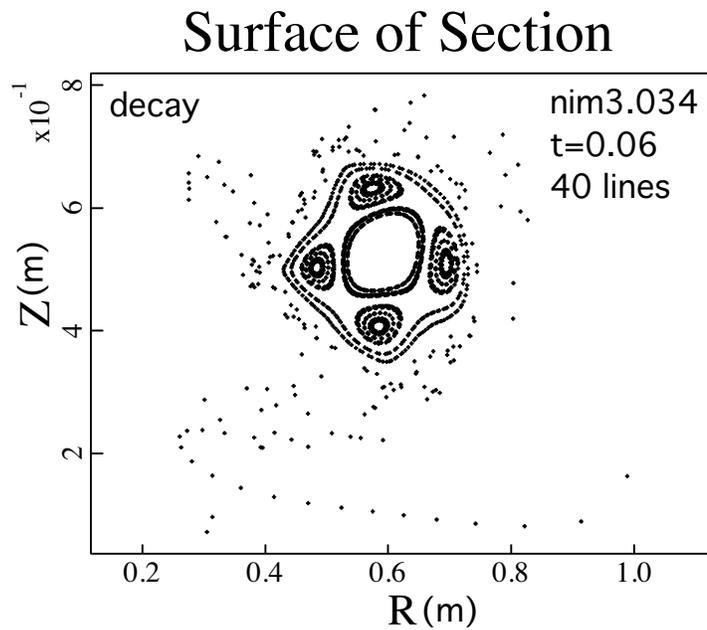


Figure 3. NIMROD toroidally averaged poloidal flux at crowbar of electrostatic drive (nim3.034).

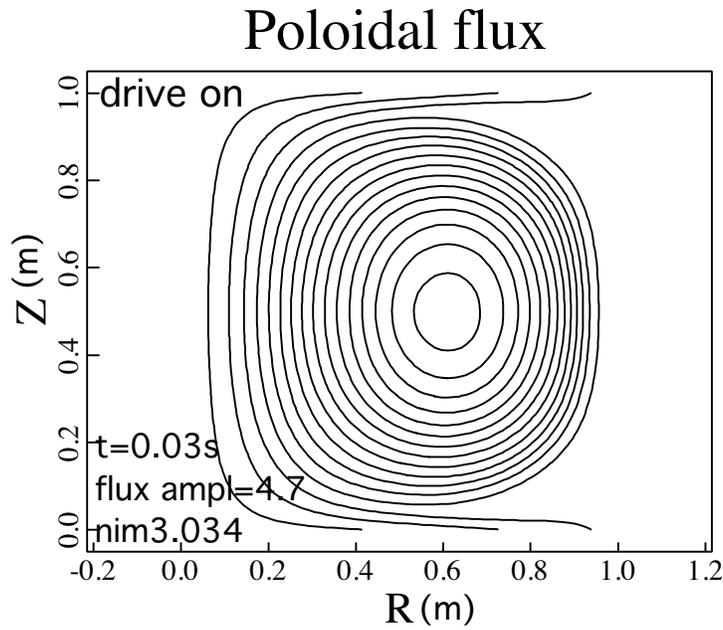


Figure 4. NIMROD magnetic energy time history during decay, resolved by toroidal Fourier harmonic (nim3.034).

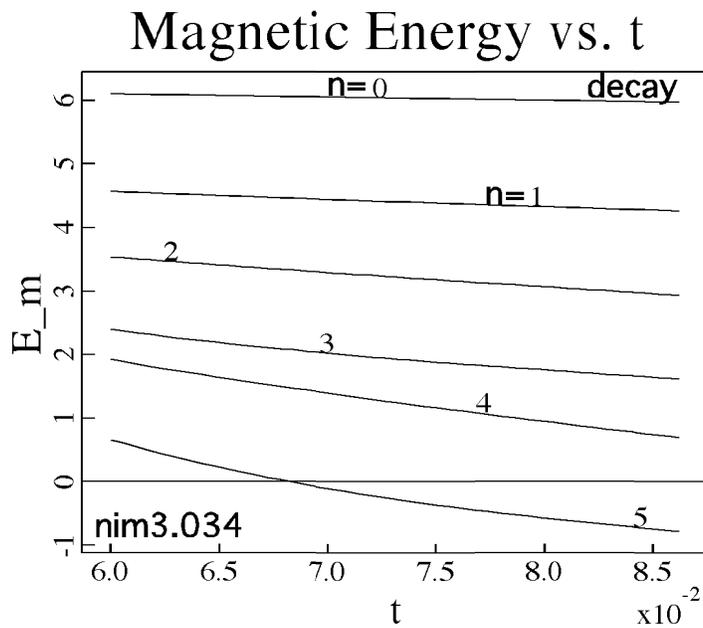


Figure 5. NIMROD simulation of decay showing peaked temperature on closed field lines (nim3.034).

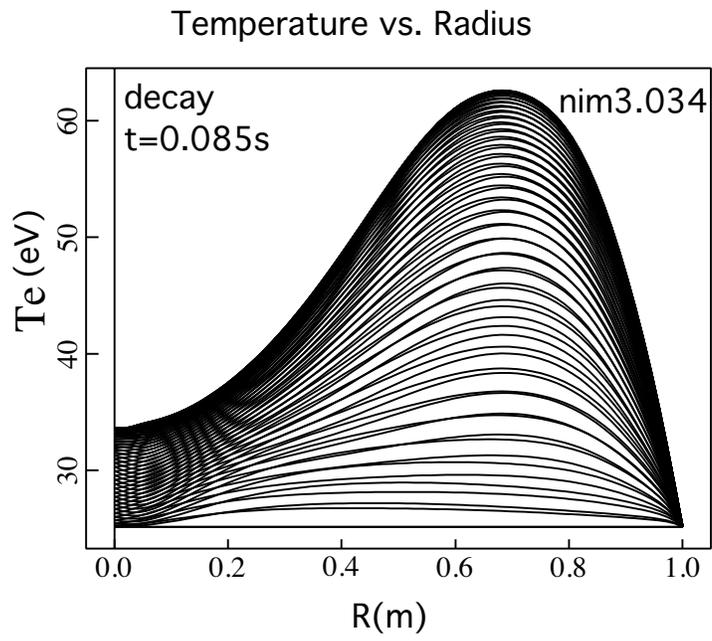
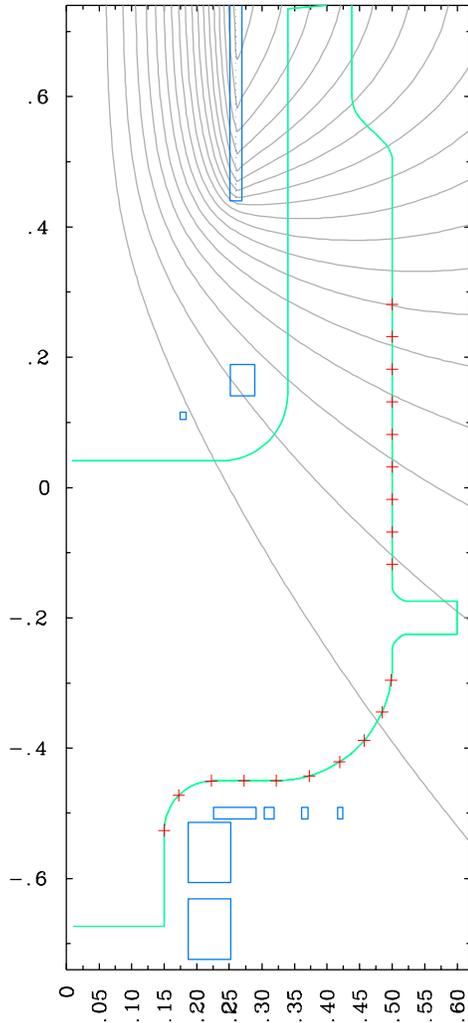


Figure 6. CORSICA plot of bias flux for SSPX vacuum field.

Bias Flux

Coil currents		
	A	I/Iref
1	0	0.00
2	0	0.00
3	0	-0.00
4	0	-0.00
5	0	0.00
6	0	0.00
7	0	0.00
8	0	-0.00
9	800	1.00

SSPX SOL vacuum field



$\Delta\Psi = 2.0$ mWb
 $\Psi_{\max} = 37.0$
 $\Psi_{\text{gun}} = 33.5$

Figure 7. CORSICA plot of SSPX equilibrium with $I_{\text{gun}}=257$ kA.

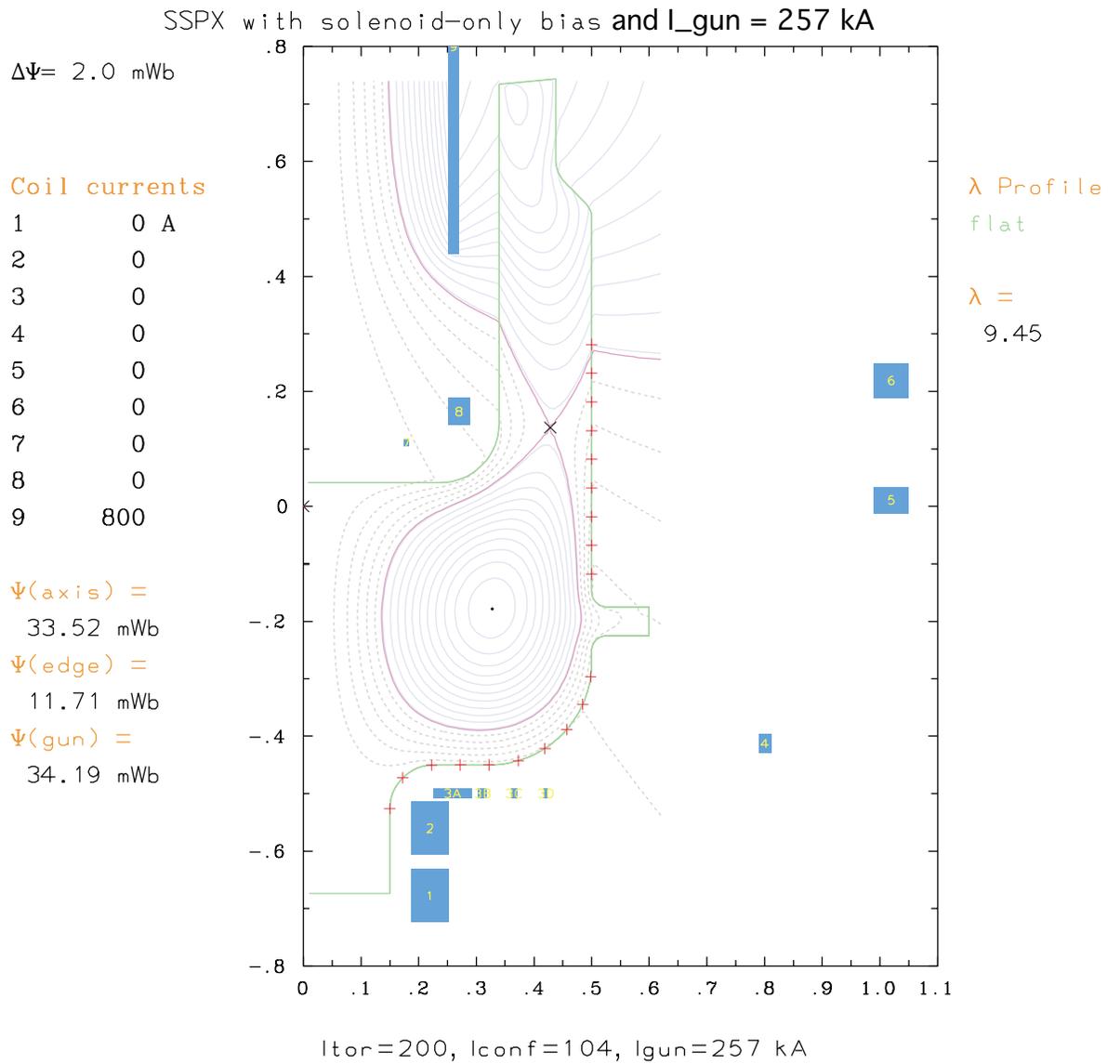


Figure 8. CORSICA plot of SSPX equilibrium with $I_{\text{gun}}=0$.

SSPX with solenoid-only bias and $I_{\text{gun}} = 0$

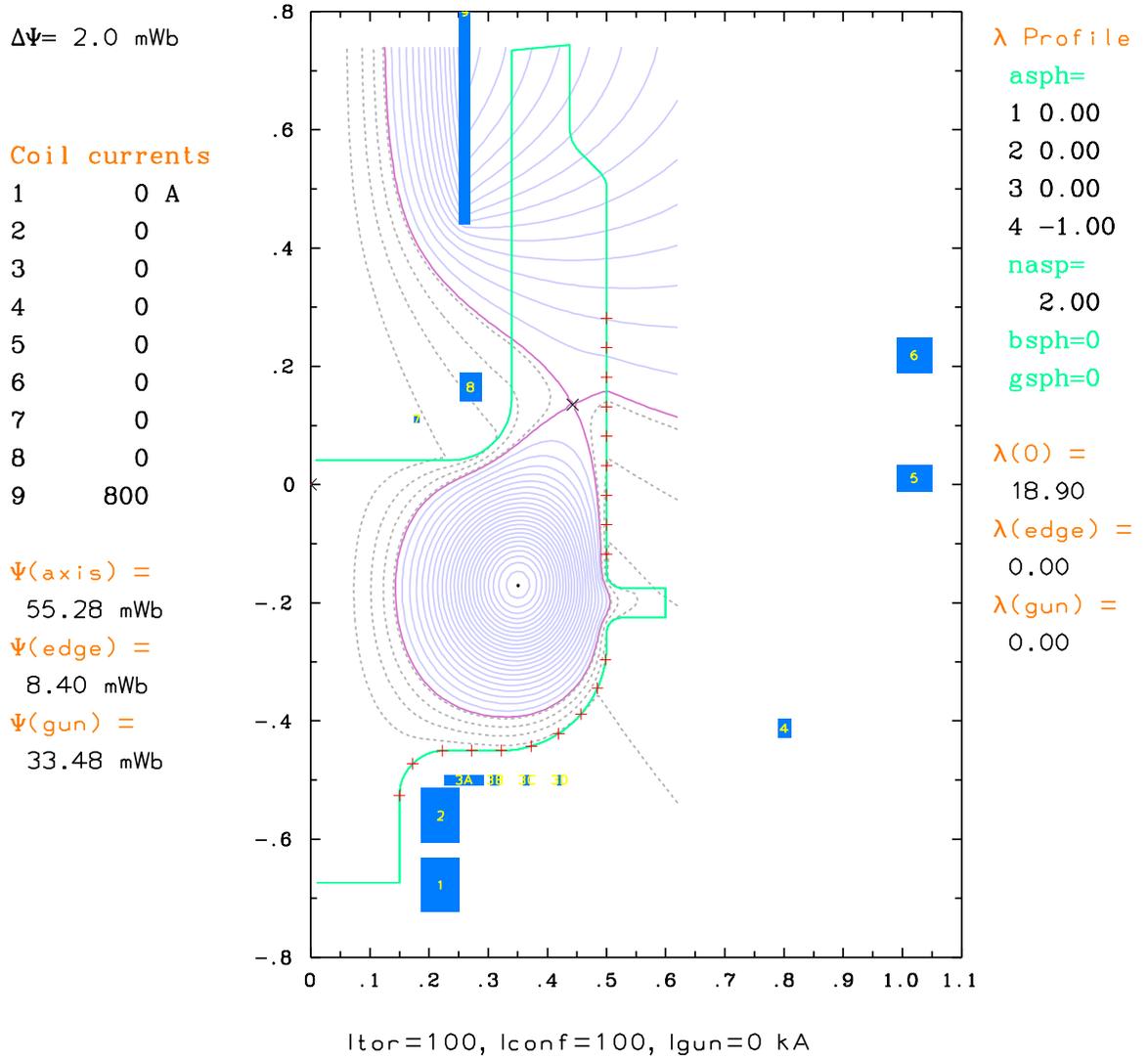


Figure 9. SPHERE calculations of delayed closure.

